

A MICROMACHINED CHEMICAL SENSOR FOR SEA FLOOR ENVIRONMENTS: INITIAL RESULTS

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ABSTRACT

This paper reports a micromachined chemical sensor intended for harsh environments such as those near hydrothermal vents at the sea floor. The sensor is intended to measure the pH, dissolved H_2 and H_2S , and temperature. The device is 12 mm in diameter and 6 mm in effective length, including packaging. A YSZ/HgO/Hg solid electrode is used as a common electrode for measurement of the three chemical quantities. The YSZ diaphragm used for this electrode is $<500 \mu\text{m}$ thick, allowing sufficient ion conductance at temperatures $>35^\circ\text{C}$. The other electrodes are thin-film metal electrodes fabricated on the same YSZ diaphragm: an Ag/AgCl reference electrode for pH sensing, an Ag/Ag₂S electrode for H_2S sensing, and a Pt electrode for H_2 sensing. The two temperature sensors are thin film Pt resistors. Initial tests have been performed to test the functionality of the pH and H_2S sensors; measurements are in line with expectations.

INTRODUCTION

In situ chemical sensing in harsh geological environments is important for many applications. One example is the exploration of hydrothermal vents located at mid-ocean ridges. On the adjacent sea floor, these vents not only create rich mineral deposits that drive mining interests, but also nurture more than 1300 previously-unknown biological species that do not depend on the sun [1]. Knowledge of chemical components and quantities, especially pH and redox (e.g. dissolved H_2 and H_2S), can provide invaluable insight into such biological communities and lead to better understanding of the bio-geochemical environments at these locations [2-3]. Rapid and direct *in situ* measurement of these quantities is essential to obtain accurate and meaningful readings. However, these measurements also present significant challenges due to high temperature and high pressure that are typical in these and other geochemical environments.

Chemical sensors designed to meet the needs in these extreme geochemical conditions are few [2-5]. A sensor based on yttria-stabilized-zirconia (YSZ) ion-conductive ceramic was reported for sensing of pH, dissolved H_2 and dissolved H_2S , and deployed at deep-sea hydrothermal vents at temperatures up to 400°C and pressure levels up to 40 MPa [2-3]. This conventional sensor had 2.5 cm diameter and >30 cm length. Reduced sensor size is desirable to allow more precise measurement of high-gradient conditions. It can also enable spatial distribution of sensor clusters to allow simultaneous characterization at multiple sites in a biological community near the vents.

This paper reports the design and initial results of a micromachined chemical sensor based on a thin YSZ diaphragm for measurement of pH, dissolved H_2 , dissolved H_2S and temperature (Fig. 1). The sensor design is intended to provide compatibility with environments that have high pressure (>10 MPa) and relatively high temperature ($\leq 150^\circ\text{C}$), such as that in a typical biological community near the vents (Fig. 2). The sensor has 12 mm diameter and ≈ 6 mm effective length with packaging. The design details are described, along with the fabrication process. Preliminary tests of the sensor have been performed in regular laboratory settings to verify the validity of the design and the functionalities of the sensor. The measurement results are

reported.

DEVICE CONCEPT

The micromachined sensor is intended to sense pH, dissolved H_2 , dissolved H_2S , and temperature. To measure the three chemical quantities, three electrochemical cells are included (Table I). The YSZ/HgO/Hg solid electrode is a common electrode used in all three electrochemical cells. It is used for pH sensing with a Ag/AgCl reference electrode. The ion conductance of the YSZ ceramic in the electrode allows measurement of the activity of H^+ ions in fluid with presence of other chemical components [6]. This electrode is also used as a reference electrode to eliminate the effect of pH on output voltage potentials, both in the measurement of dissolved H_2 with a Pt sensing electrode, and in the measurement of dissolved H_2S with a Ag/Ag₂S sensing electrode. The voltage potential between the electrodes in each cell is related

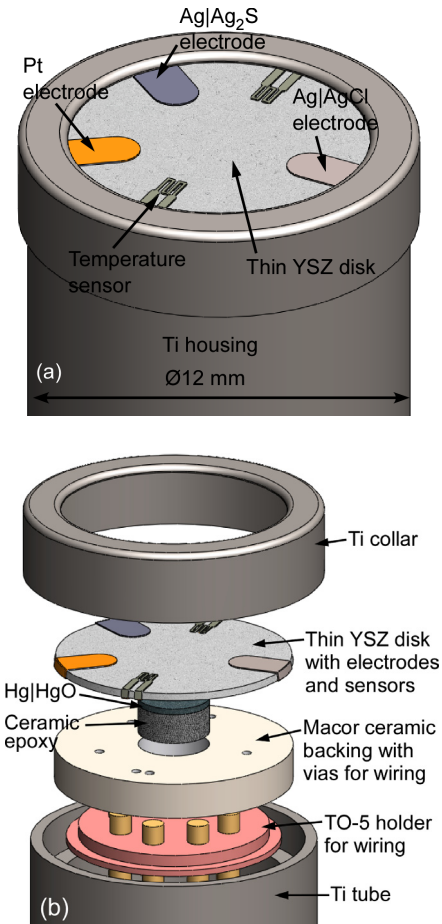


Figure 1: Schematics of the micromachined sensor proposed for analysis of geofluids in harsh environments. (a) Perspective view of the full device, showing sensing electrodes and temperature sensors (RTDs) on the thin YSZ disk and the $\Phi 12$ mm titanium housing. (b) Exploded view showing individual components inside the Ti housing.

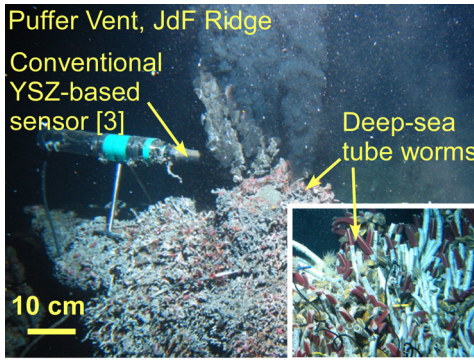


Figure 2: Exploration of deep sea hydro-thermal vents using manned submersible assets [3]. Photo shows deployment of a conventional YSZ-based sensor unit at Puffer Vent of Juan de Fuca Ridge.

Table I: Electrochemical cells and their corresponding electrodes in the micromachined chemical sensor.

Sensing target	Electrochemical cell
pH	Ag AgCl Target solution YSZ HgO Hg
Dissolved H ₂	Pt Target solution YSZ HgO Hg
Dissolved H ₂ S	Ag Ag ₂ S Target solution YSZ HgO Hg

to the corresponding target chemical quantity by [3,7]:

$$V_{pH,T,P} = V_{pH}^0 - \frac{2.303RT}{F} \left(\log a_{Cl^-} - \frac{1}{2} \log a_{H_2O} - pH_i \right) \quad (1)$$

$$V_{H_2,T,P} = V_{H_2}^0 + \frac{2.303RT}{2F} \log \left(\frac{K_H \cdot \gamma_{H_2} \cdot m_{H_2}}{a_{H_2O}} \right) \quad (2)$$

$$V_{H_2S,T,P} = V_{H_2S}^0 + \frac{2.303RT}{2F} \log \left(\frac{K_H \cdot \gamma_{H_2S} \cdot m_{H_2S}}{a_{H_2O}} \right) \quad (3)$$

where $V_{pH,T,P}$, $V_{H_2,T,P}$, $V_{H_2S,T,P}$ are measured voltage potentials at corresponding cells, V_{pH}^0 and $V_{H_2S}^0$ are the standard cell potentials at the appropriate temperatures and pressure and the values can be determined from the standard state potentials of Ag|AgCl, Ag|Ag₂S and Hg|HgO electrodes (i.e. $V_{Ag|AgCl}^0$, $V_{Ag|Ag_2S}^0$ and $V_{Hg|HgO}^0$, respectively), a is the activity of the chemical component, R is the gas constant, F is the Faraday constant, T is temperature in K, pH_i is the pH to be measured, K_H is the Henry's law constant, γ_{H_2} and γ_{H_2S} are the activity coefficients of H₂ and H₂S, and m_{H_2} and m_{H_2S} are the dissolved H₂ and H₂S concentrations, respectively. With a DC measurement of the corresponding cell potential at the target temperature and pressure, direct sensing of each chemical quantity can be obtained. Temperature sensing is performed by two Pt-film resistance-temperature-detectors (RTD) through a measurement in resistance change of the Pt films.

The schematics of the sensor design are shown in Fig. 1 and Fig. 3. All sensor components are integrated at the end of a titanium tube. A thin YSZ disk/diaphragm is used for ion conduction to the underneath Hg|HgO paste electrode. The thickness of the YSZ disk should be small enough ($\ll 1$ mm) to allow sufficient ion conduction for the sensing purpose at temperatures below 100°C. The disk is also a common substrate for other thin metal-film electrodes (Ag|AgCl, Pt and Ag|Ag₂S) and RTDs. Electrical connections from these electrodes/RTDs run over a 10°-tapered sidewall of the YSZ disk to the backside. No through-hole or cavity is present on the YSZ surface to avoid leakage under pressure. The YSZ disk is supported by a Macor®

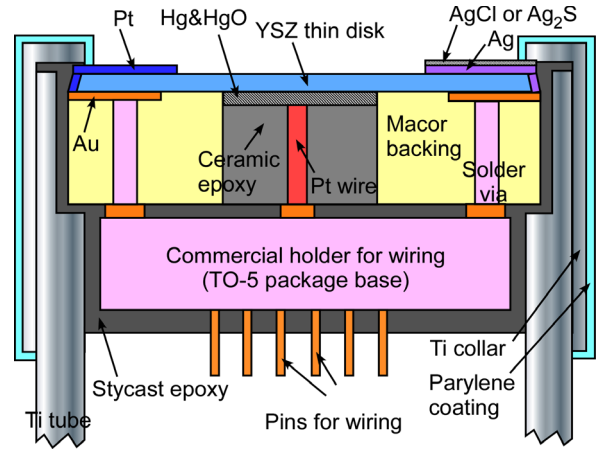


Figure 3: Schematic of the micromachined sensor in 2D cross-sectional view, showing integration of individual components. Note that parylene is selectively coated on the sensor external surface, covering RTDs but not other electrodes.

ceramic disk, which has feedthroughs for electrical connection from the backside of the YSZ disk to a commercial TO-5 holder for cable wiring. The Hg|HgO paste is sealed inside a cavity in the Macor disk by ceramic epoxy, with a Pt wire going out for electrical connection (Fig. 3). The Ti tube covers all sidewalls of internal components, and a Ti collar wraps around the edge of the YSZ front surface, minimizing potential leak path. High-strength vacuum-sealing Stycast epoxy encapsulates all internal components and seals the Ti housing. Selective coating of parylene or other polymers provides additional device sealing and electrical insulation for RTDs.

DEVICE FABRICATION

The YSZ disks were custom-made using Type ZDY-4 material (CoorsTek, Inc., CO, USA). In order to deposit thin-film metal electrodes/RTDs on the surface of the YSZ disk, a shadow mask was used. The metal films, including Pt and Ag on the front side and Au on the backside of the disk, were sequentially deposited by sputtering or evaporation through the corresponding patterns on the shadow mask. The thicknesses of the metal films are 200/1000 Å for Ti/Pt, and 500/20000 Å for Ti/Ag, and 500/5000 Å for Ti/Au. Features were included on the shadow

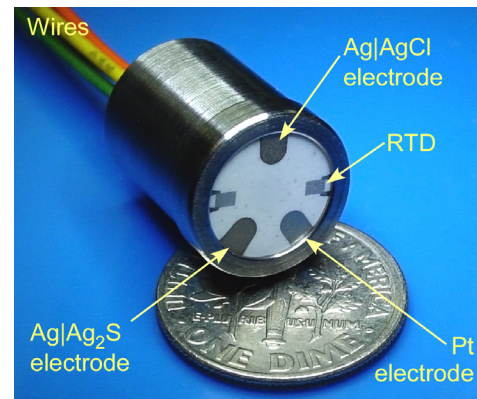


Figure 4: Photo of an integrated device on a US dime, showing Ag|AgCl, Ag|Ag₂S and Pt electrodes and 30 μm-wide Pt lines for RTDs, before selective parylene coating. The 15 mm length of the Ti tube is for demonstration only. Effective sensor length from YSZ disk to TO-5 holder: ≈6 mm.

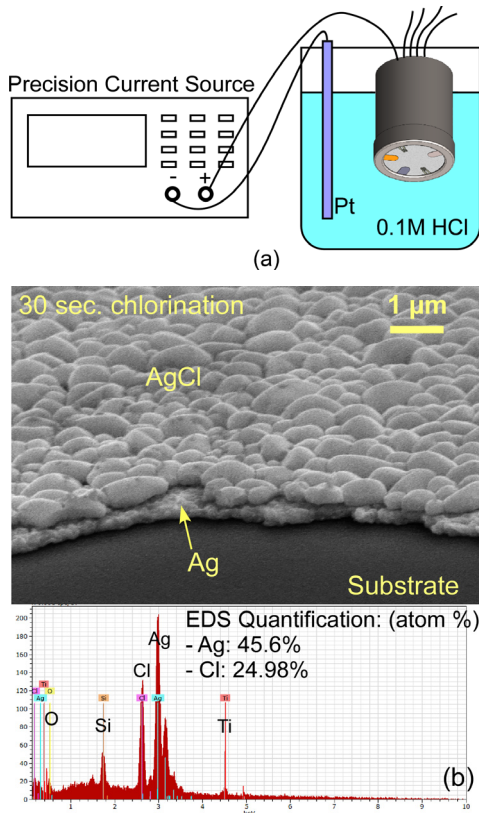


Figure 5: (a) Setup for silver chlorination. The counter electrode is a silicon wafer evaporation-coated with 5000 Å platinum. Current density: 2 mA/cm². (b) SEM image and EDS analysis result of the chlorinated Ag film on a glass test substrate.

mask to allow alignment between different metal films. The thin-film RTDs consist of 30 μm-wide folded Pt lines and have a resistance of ≈200 Ω each. The 10°-tapered edge of the YSZ disk allowed metal to be deposited on the slope to make the electrical connection to the backside of the disk.

The HgIHgO paste was formed by mixing Hg (99.9998% purity) and HgO (99.998% purity) (Alfa Aesar, MA, USA). The Macor ceramic disk was custom-made by micromilling using material obtained from McMaster, NJ, USA. The disk has a thickness of 1.588 mm. The center cavity on the disk for HgIHgO paste and ceramic epoxy has a diameter of 3 mm. The electrical feedthroughs/vias have a diameter of 500 μm. The Ti tube and collar were custom-machined from Grade 5 Ti alloy (Ti-6Al-4V, McMaster, NJ, USA), which has excellent mechanical strength and corrosion resistance. A photo of an integrated device is shown in Fig. 4. The effective length of the sensor from the YSZ disk to the TO-5 holder is ≈6 mm.

After the sensor components were integrated, the 2 μm-thick Ag films on the YSZ disk were activated by chlorination and sulfurization, turning the Ag films into AgI/AgCl and AgI/Ag₂S electrodes, respectively. For silver chlorination, the sensor was dipped into an HCl solution with a concentration of 0.1 M (Fig. 5a). The counter electrode was a silicon wafer with an evaporated 5000 Å-thick Pt film. The current density used for chlorination was 2 mA/cm². This current level has been reported to provide a uniform coating of AgCl with a grain size around 1 μm [8]. For silver sulfurization, an electrochemical cell of AgI/AgCl|S²⁻|Ag₂S|Ag was formed. The electrodes in the cell were a separately-built AgI/AgCl electrode and the target Ag film on the sensor; a

Na₂S solution was used as the electrolyte. The AgI/AgCl electrode that was formed on the sensor was protected by a photoresist coating. The target Ag film on the sensor was sulfurized by externally shorting the cell.

EXPERIMENTAL RESULTS

The chlorination procedure was characterized using a Ag film coated on a glass substrate. This Ag film was deposited by sputtering in the same session when the Ag films on the YSZ disks were deposited. The obtained AgI/AgCl film is shown in the upper portion of Fig. 5(b). The AgCl layer has a grain size of ≈1 μm as expected and is uniformly coated on the remaining Ag layer. Energy dispersive spectroscopy (EDS) was done to characterize the electrode and the obtained spectrum is shown in the lower portion of Fig. 5(b). According to the EDS quantification result, the electrode has 45.6% atom percentage for Ag and 24.98% for Cl, suggesting a ratio of ≈1 between Ag and AgCl.

As a common electrode for all three chemical sensing functions, the YSZ|HgO|Hg solid electrode is the core component of the sensor. It also presented the most challenge in the fabrication of all four electrodes. pH measurements in a regular laboratory setting using this electrode can provide direct verification of its integrity and functionality. In these measurements, hydrochloric acid solutions with pH ranging in 2-5.5 were used. The pH values were verified with a double-junction pH meter (Oakton® pHTestr 3+), which has an accuracy of 0.1. Before it was used, the meter was calibrated with certified pH buffer solutions from Fisher Scientific. The HCl solutions were heated on a hotplate to 35°C, and a thermocouple was used to monitor the solution temperature. The voltage potential between the AgI/AgCl and YSZ|HgO|Hg electrodes on the sensor was read out by an Agilent 34401A multimeter with its input resistance set at >10 GΩ.

As shown in Fig. 6, the plot of measured $V_{pH,T,P}$ vs. pH has a slope of 123.2 mV/pH. This slope is about double the Nernst slope of 61.14 mV/pH at 35°C. This is due to the presence of both H⁺ and Cl⁻ ions in the solutions. The YSZ|HgO|Hg electrode is sensitive to H⁺ ions while the AgI/AgCl electrode is sensitive to Cl⁻ ions. In a regular laboratory environment, the strong HCl acid can generate equal concentrations of H⁺ and Cl⁻ in the solution

$$\log a_{Cl^-} = \log a_{H^+} = -pH_t \quad (4)$$

Assume the activity of H₂O in the regular lab environment is 1,

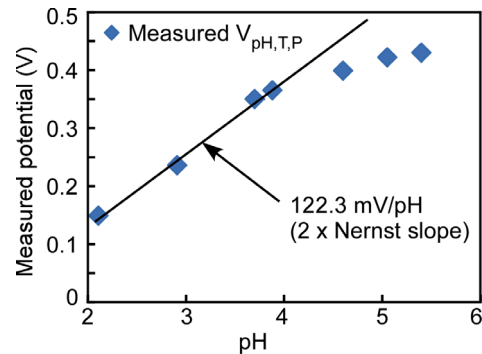


Figure 6: Measured potential between the AgI/AgCl and YSZ|HgO|Hg electrodes, vs. pH of HCl solutions at 35°C. The straight line plots double the Nernst slope of 61.14 mV/pH at 35°C for comparison. This slope is due to the effect of both H⁺ and Cl⁻. For pH>4, $V_{pH,T,P}$ saturates. This may be due to activity of H⁺ and OH⁻ from H₂O at higher pH, and also of low Cl⁻ for AgI/AgCl electrode.

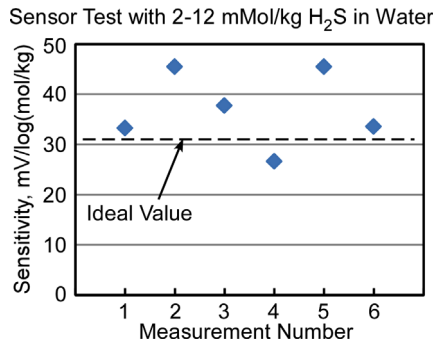


Figure 7: Sensitivity of measured sensor responses to the H_2S concentration in water, and comparison to the ideal value of 30.6 mV/log(mol/kg). The sensor output potential was taken between the YSZ|Hg|OHg and Ag|Ag₂S electrodes at 35°C. Differences from the ideal value are related to uncertainty in the H_2S concentration.

$$\log a_{H_2O} = 0 \quad (5)$$

Equation (1), which provides the relationship between the measurement voltage potential and pH, can be simplified as

$$V_{pH,T,P} = V_{pH}^0 + 2 \cdot \frac{2.303RT}{F} \text{pH}_1 \quad (6)$$

This indicates that the expected slope of $V_{pH,T,P}$ vs. pH is double the Nernst slope. At 35°C, the expected slope is 122.3 mV/pH, and the measured value is comparable to it. This indicates the validity of the pH sensor design and the integrity of the YSZ|Hg|OHg core electrode.

Also shown in Fig. 6, $V_{pH,T,P}$ saturates at pH values ≥ 4 . This may be due to activity of H^+ and OH^- from H_2O at higher pH, and also low Cl^- activity at low HCl concentration for the Ag|AgCl electrode.

H_2S sensing was tested using hydrogen sulfide water (Grainger, Inc., USA) with varying concentration estimated in the range of 2-12 mMol/kg. The sensor output potential was taken between the YSZ|Hg|OHg and Ag|Ag₂S electrodes at 35°C. The sensitivity of the sensor - i.e. the change in output potential per unit change in the H_2S concentration - was typically 26-45 mV/log(mol/kg) (Fig.7). The ideal value is 30.6 mV/log(mol/kg) according to Equation 3. Differences from the ideal value are related to uncertainty in the H_2S concentration, which can vary from the estimated value due to reasons such as oxidation of dissolved sulfide into sulfate.

DISCUSSION

As described in the experimental results, the sensor responds to both H^+ and Cl^- concentrations in the pH measurement without a buffer solution that provides a constant Cl^- concentration for the Ag|AgCl electrode. This makes it difficult to use the sensor in regular applications, though approaches such as a coating of KCl gel on the Ag|AgCl electrode can provide simple solutions [8]. However, in the target environments at hydrothermal vents, the sea water presents a saturated Cl^- concentration that is mostly constant, rendering these additional techniques unnecessary.

The sensor has been tested for pH and H_2S measurement in a laboratory environment. Although the sensor is designed for high pressure and relatively high temperature applications, its

performance in harsh environments remains to be evaluated. This, together with the sensing function for dissolved H_2 and temperature, will be verified in future efforts.

CONCLUSIONS

A micromachined chemical sensor intended for applications in harsh environments has been design and implemented. Sensing functions for pH, dissolved H_2 and H_2S , and temperature are included. Techniques for silver chlorination and sulfuration have been developed and characterized to activate the Ag|AgCl reference electrode for pH sensing and the Ag|Ag₂S sensing electrode for H_2S sensing. Initial measurement results for pH and H_2S sensing in a regular laboratory environment indicate validity of the sensor design and the integrity of the YSZ|Hg|OHg core component. Further characterization of sensor functions as well as device testing under harsh environments will be pursued in future effort.

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